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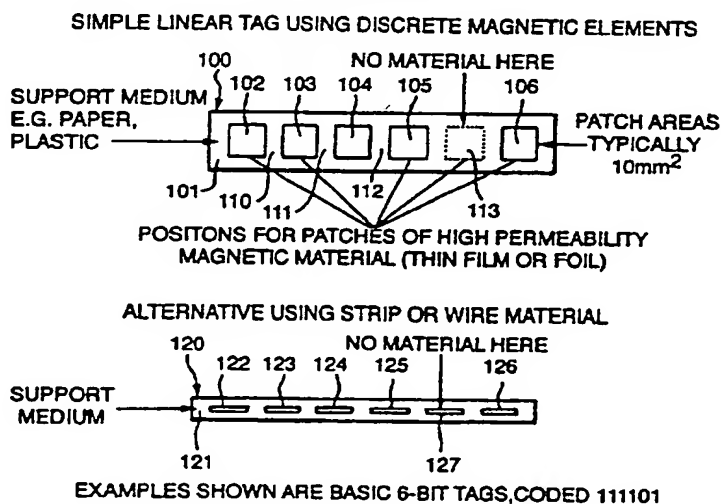
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(54) Abstract Title

Magnetic Tags

(57) A magnetic marker or tag comprises a substrate carrying a plurality of discrete magnetically active regions disposed in one or more linear arrays. The magnetically active regions are formed of a thin film or spin-melt material having a preferential axis of magnetisation, and the preferential axis of magnetisation is aligned within the (or each) linear array.

Fig.9a.



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Fig.1.

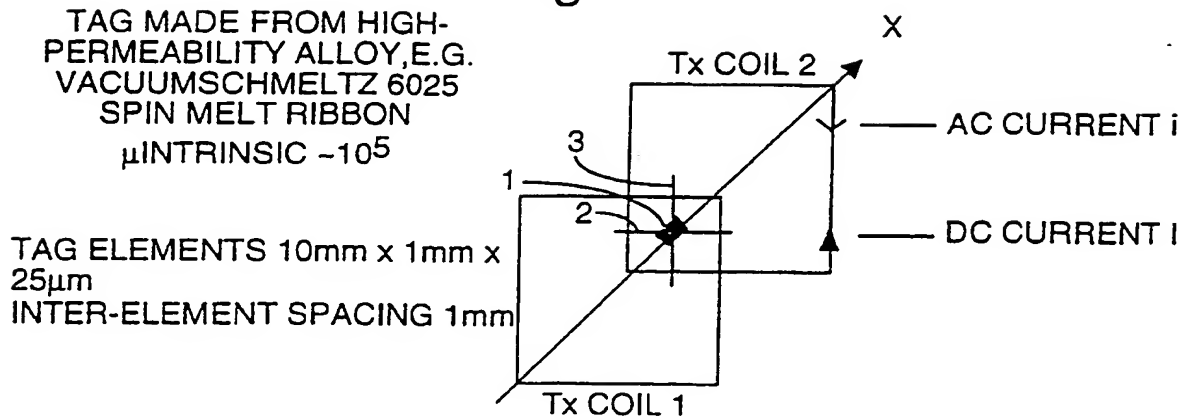


Fig.2.

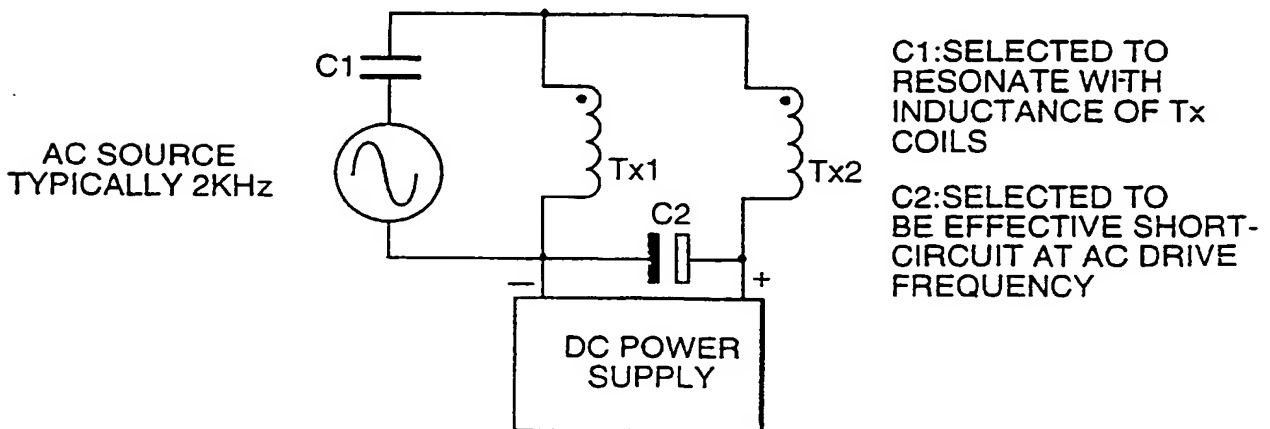


Fig.3a.

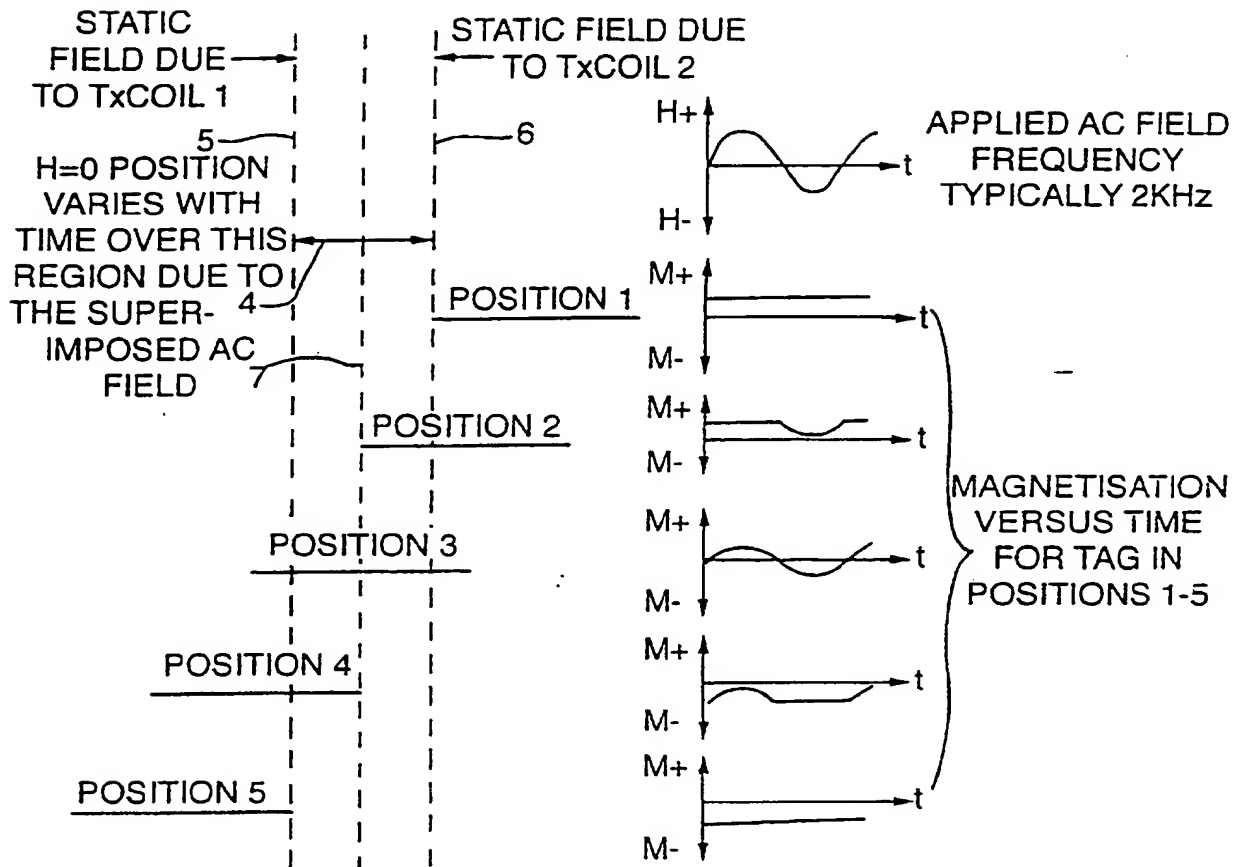


Fig.3b.

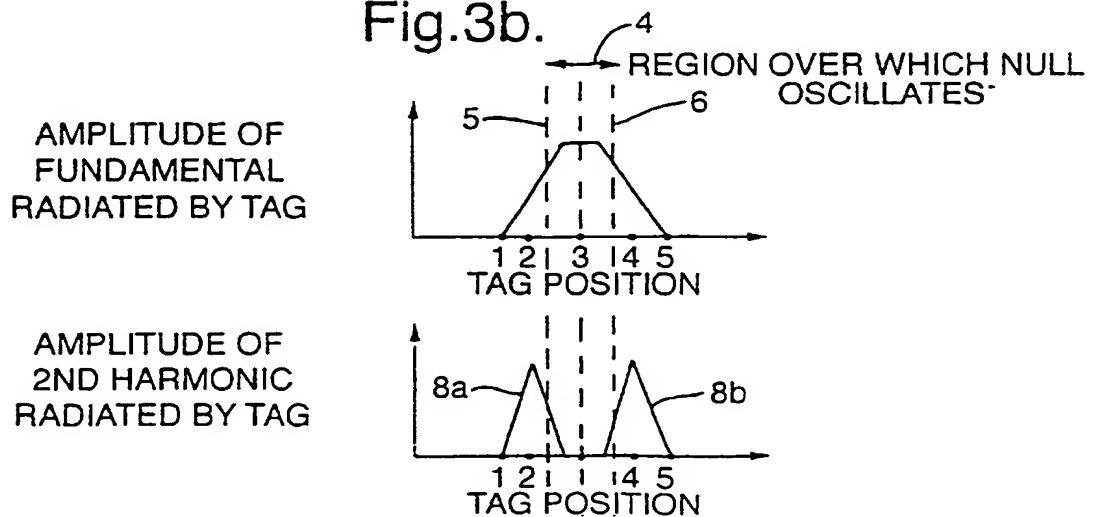
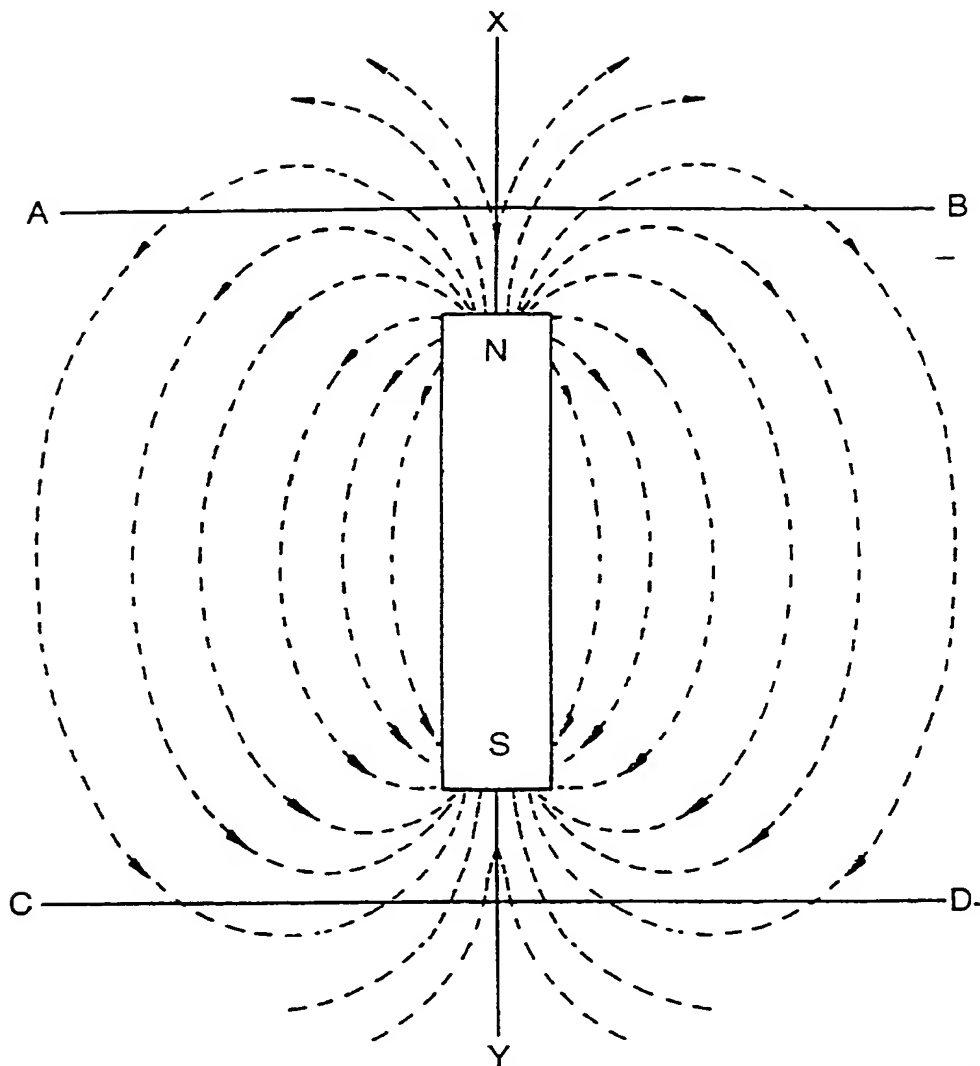
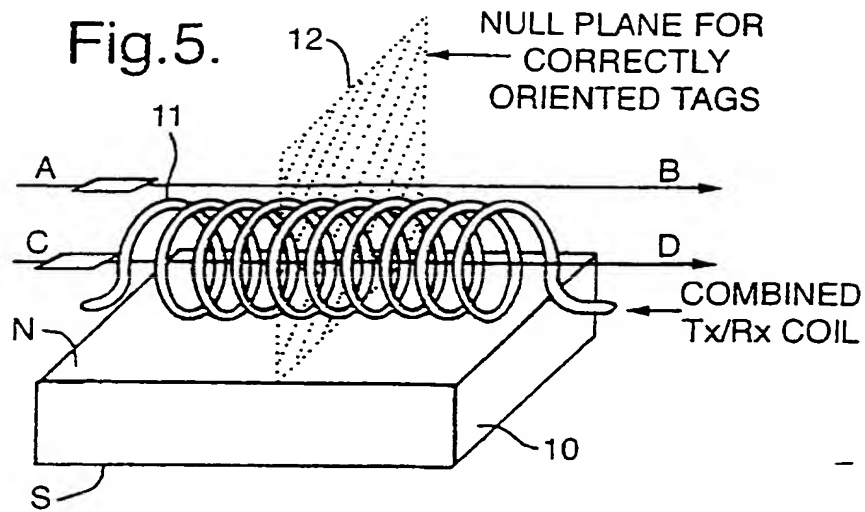


Fig.4.



A SIMPLE BAR-MAGNET HAS REGIONS NEAR TO ITS POLES WHERE NARROW NULL PLANES EXIST FOR TAGS WITH THEIR SENSITIVE AXES ALIGNED ORTHOGONAL TO X-Y. PATHS A-B OR C-D CAN BE USED AS THE BASIS OF A SIMPLE INTERROGATOR.



TAGS MAY PASS EITHER THROUGH COIL (PATH C-D) OR OVER COIL (PATH A-B)

TAGS MUST BE ORIENTED WITH THEIR MAGNETIC AXIS IN THE DIRECTION OF THE TAG MOVEMENT

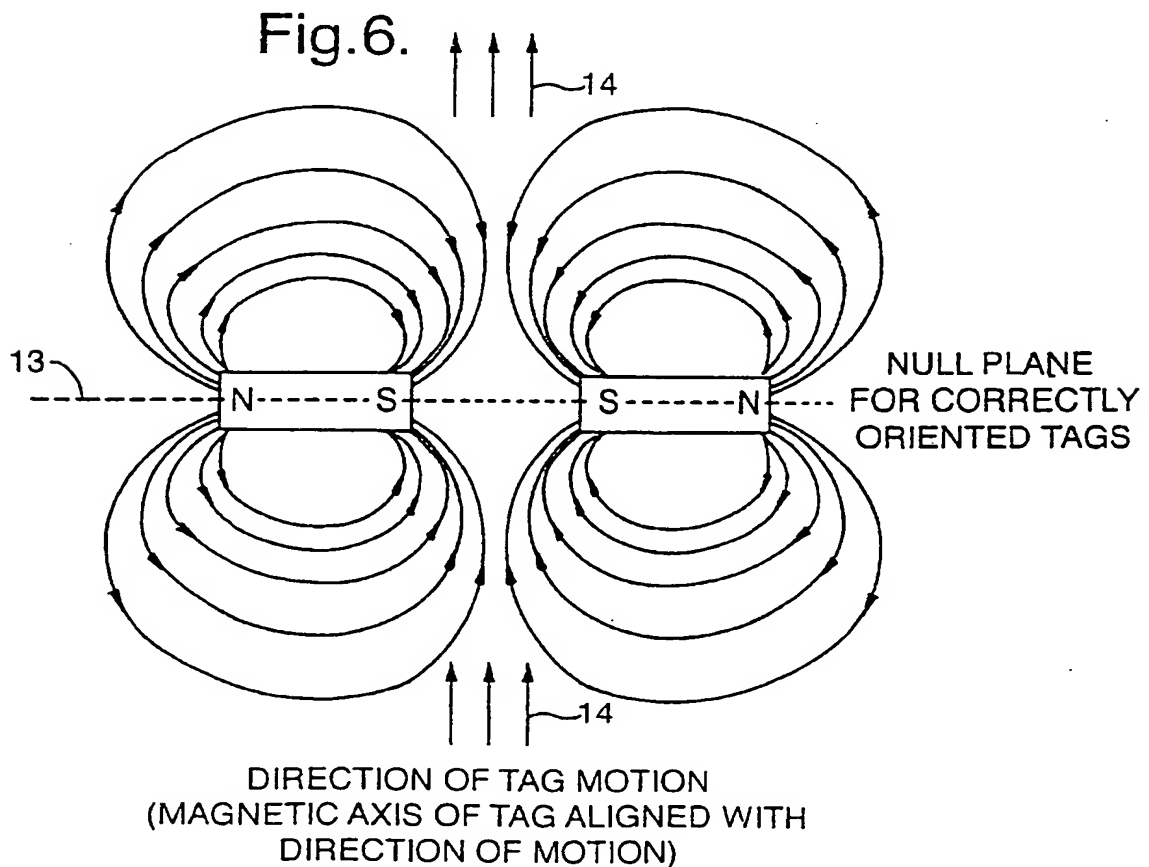


Fig.7.

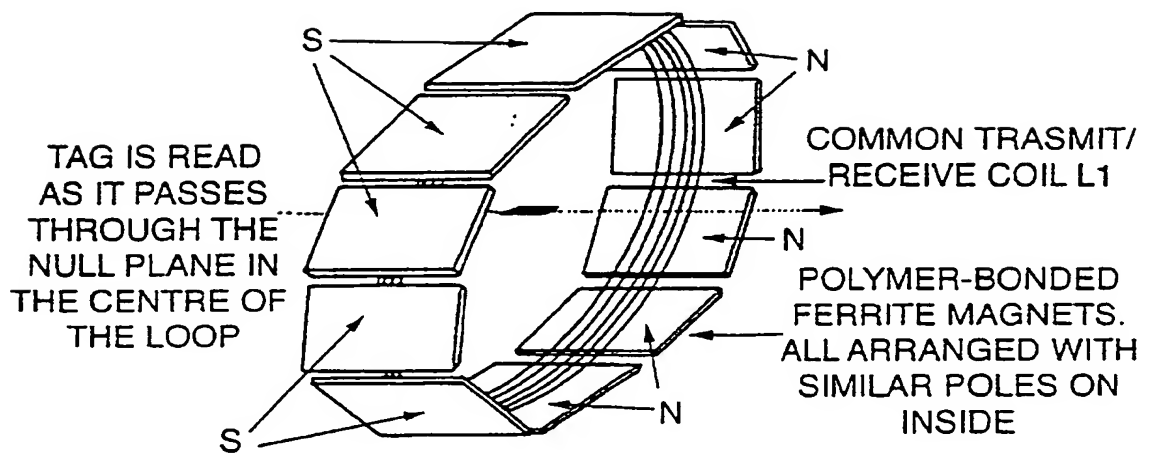
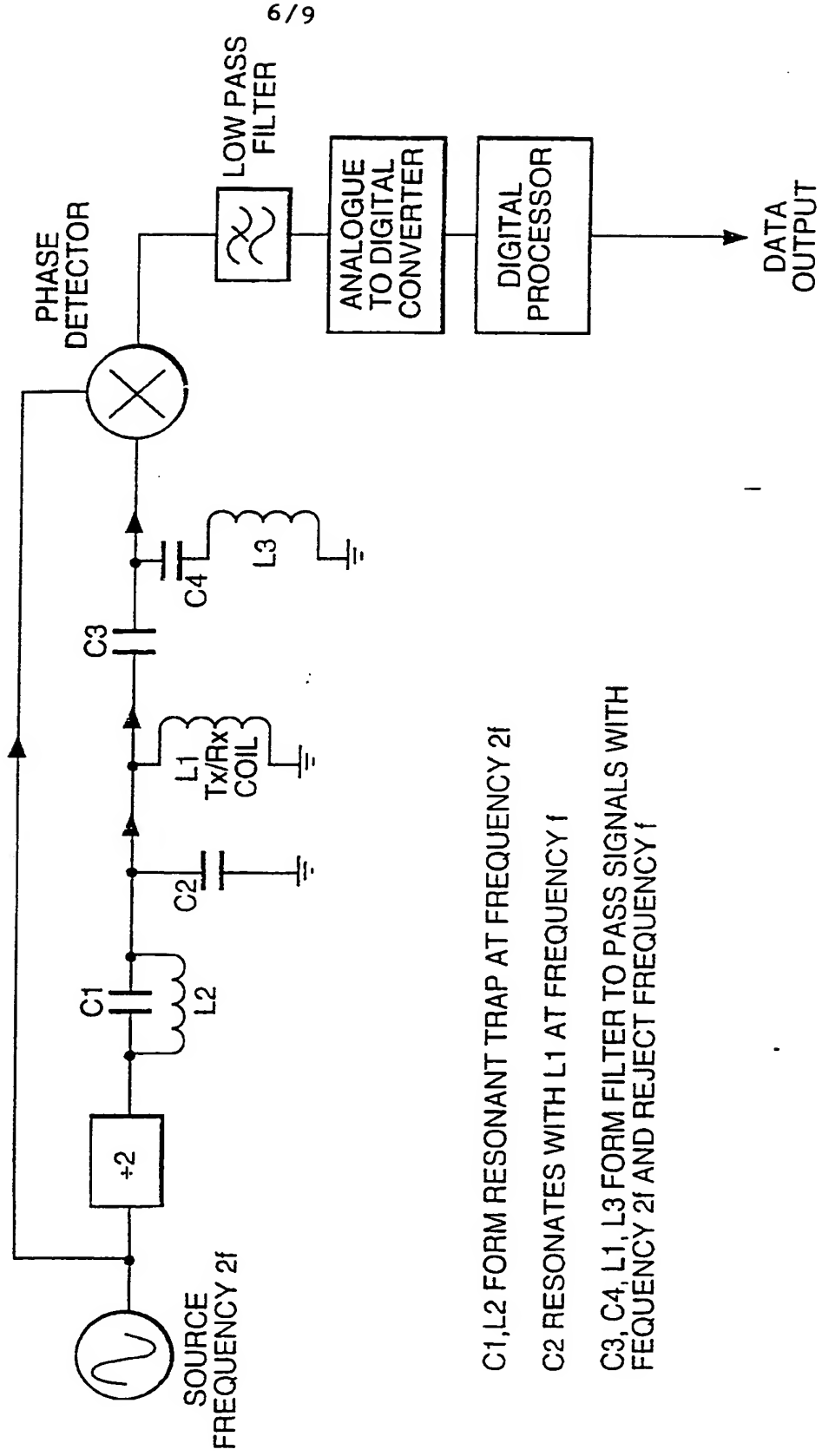
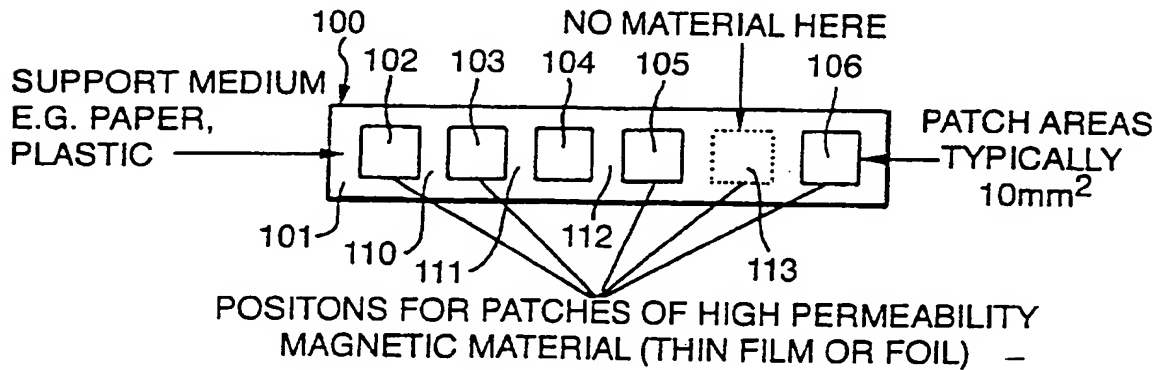


Fig.8.

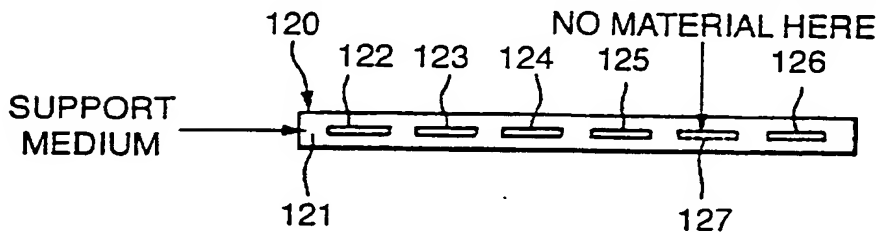


7/9  
Fig.9a.

# SIMPLE LINEAR TAG USING DISCRETE MAGNETIC ELEMENTS



## ALTERNATIVE USING STRIP OR WIRE MATERIAL



EXAMPLES SHOWN ARE BASIC 6-BIT TAGS, CODED 111101

Fig.9b.

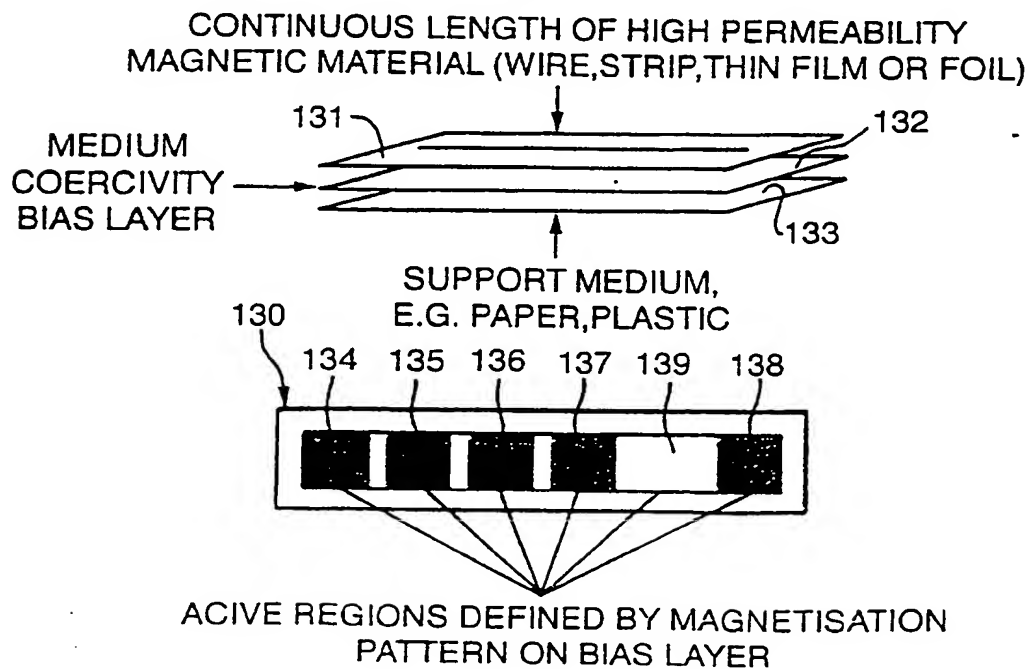
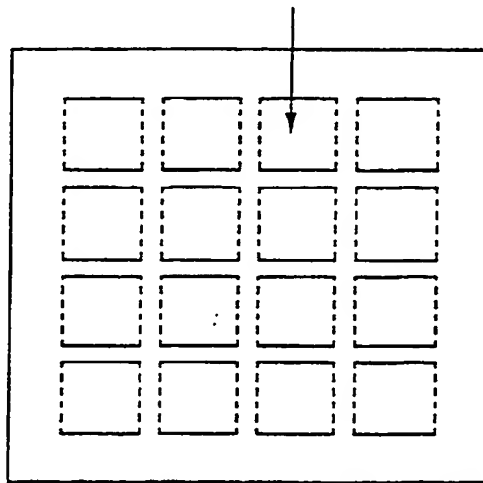




Fig.9c.

POSITION WHERE DISCRETE ELEMENT MAY BE PLACED, OR  
HIGH PERMEABILITY REGION CAN BE DEFINED  
(MAGNETICALLY, USING BIAS LAYER OR BY OTHER METHODS)



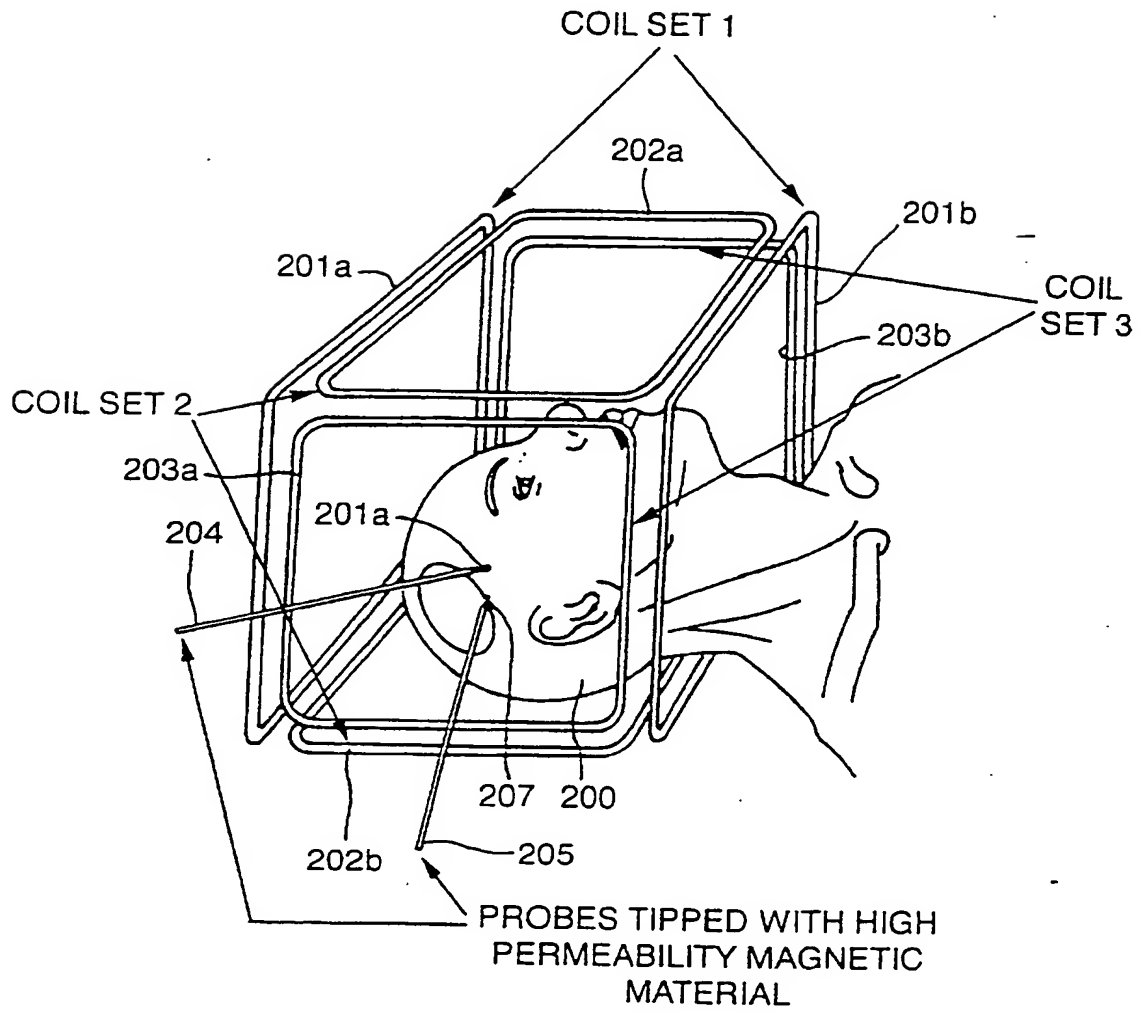
16-BIT TAG

Fig.9d.



TYPICAL DETECTED OUTPUT FROM READER (ADC INPUT)

Fig.10.



MAGNETIC MARKERS OR TAGS

This application is divided out of Application No. 9713224.5 (hereinafter termed "the parent application") and relates to magnetic markers or tags.

The parent application relates to the exploitation of magnetic properties in a range of practical techniques, and utilises a new technique of spatial magnetic interrogation in conjunction with a magnetic marker or identification tag. More particularly, it relates to methods of determining the presence and/or the location of a magnetic marker or tag within an interrogation zone; to methods of identifying a magnetic tag (e.g. identifying a given tag in order to discriminate that tag from others); to systems for putting these methods into practice; to magnetic tags for use in such methods and systems; and to the storage of data in such tags, and the subsequent remote retrieval of data from such tags.

It should be understood that the terms "tag" and "marker" are used herein interchangeably; such devices may be used in many different applications and, depending on the magnetic qualities of the device, may serve to denote (a) the mere presence of the tag (and hence that of an article to which the tag is attached); or (b) the identity of the tag (and hence that of an article to which it is attached); or they may serve to define the precise position of the tag with respect to predetermined co-ordinates (and hence that of an article to which it is attached); or they may serve to provide access codes (e.g. for entry into secure premises; or for ticketing purposes, e.g. on public transport networks); or they may serve generally to discriminate one article or set of articles from other

articles.

In addition, the terms "ac field" and "DC field" are used herein to denote magnetic fields whose  
5 characteristics are, respectively, those associated with an electrical conductor carrying an alternating current (ac) or a direct current (DC).

The methods and systems of the invention disclosed  
10 in the parent application have a wide variety of applications as indicated above. These include (but are not restricted to) inventory control, ticketing, automated shopping systems, monitoring  
work-in-progress, security tagging, access control,  
15 anti-counterfeiting, and location of objects (in particular the precise positioning of workpieces [e.g. probes in surgery]). Full details of the magnetic interrogation technique on which these various practical applications are based are found in the  
20 parent application (GB9713224.5) and in International Patent Application No. PCT/GB97/00823 (published as WO 96/31790 and hereinafter referred to as "the PCT application") from which it is derived.

25 There are a number of passive data tag systems currently available. The most widely-used is based on optically-read printed patterns of lines, popularly known as barcodes. The tag element of such systems is very low-cost, being typically just ink and paper. The  
30 readers are also relatively low cost, typically employing scanning laser beams. For many major applications the only real drawback to barcodes is the need for line-of-sight between the reader and the tag.

35 For applications where line-of-sight is not possible, systems not employing optical transmission

have been developed. The most popular employ magnetic induction for coupling between the tag and the interrogator electronics. These typically operate with alternating magnetic fields in the frequency range of 5 50kHz to 1MHz, and generally employ integrated electronic circuits ("chips") to handle receive and transmit functions, and to provide data storage and manipulation. In order to avoid the need for a battery, power for the chip is obtained by 10 rectification of the interrogating signal received by an antenna coil. In order to increase the power transferred, and to provide discrimination against unwanted signals and interference, the coil is usually resonated with a capacitor at the frequency of the 15 interrogation signal carrier frequency. A typical product of this type is the TIRIS system manufactured by Texas Instruments Ltd.

Other multi-bit data tag systems have employed 20 conventional h.f. radio technology, or technologies based on surface acoustic waves or magnetostriction phenomena.

The invention disclosed in the PCT application 25 involves, *inter alia*, the use of a new type of passive data tag system which employs small amounts of very high-permeability magnetic material, and a scanned magnetic field for interrogation. Since the magnetic material can be in the form of a thin foil, wire or 30 film, it can be bonded directly to a substrate, e.g. paper or a plastics material, to form self-supporting tags.

Alternatively, the magnetic material may be 35 incorporated into the structure of an article with which the tag is to be associated; thus a tag may be

formed *in situ* with the article in question by applying the magnetic material to the surface of the article, or by embedding the magnetic material within the body of the article.

5

The invention described and claimed in the parent application exploits magnetic fields which contain a "magnetic null" - this term is used herein to mean a point, line, plane or volume in space at or within  
10 which the component of the magnetic field in a given linear direction is zero. The volume in space over which this condition is met can be very small - and \_ this gives rise to certain embodiments of the parent invention in which precise position is determined.  
15 Typically the magnetic null will be extant over a relatively small linear range. It should be understood that, where there is a magnetic null, it is possible (and is often the case) that the magnetic field component in a direction orthogonal to the given linear  
20 direction will be substantial. In some embodiments of the interrogation system, such a substantial orthogonal field is desirable.

One way of creating the magnetic null is to employ  
25 opposing magnetic field sources. These may be current-carrying coils of wire, or permanent magnets (these being well suited to small-scale systems), or combinations of coil(s) and permanent magnet(s). It is also possible to exploit the magnetic nulls which exist  
30 in specific directions when a single coil or permanent magnet is used.

For large scale applications, the magnetic field sources are preferably coils carrying direct current.  
35

The invention described and claimed in the parent

application also utilises the relative movement between a magnetic marker and an applied magnetic field in order to effect passage over of the marker of the magnetic null. This can be achieved by moving the  
5 marker with respect to the applied magnetic field, or by holding the marker in a fixed position while the magnetic field is scanned over it. Generally, the interrogation technique exploits the difference between the magnetic behaviour of the marker in (i) a zero  
10 field (at the magnetic null), and (ii) in a high, generally saturating, magnetic field.

The parent application describes and claims a method of interrogating a magnetic element having non-  
15 linear magnetic properties, which is characterised by the steps of: (1) applying a magnetic field to a region where the magnetic element is, or is expected to be, located, which results in a magnetic null as defined above within said region; (2) causing relative movement  
20 between said magnetic field and said magnetic element such that the magnetic element traverses the magnetic null, or vice versa; and (3) detecting the magnetic response of the magnetic element during said relative movement.

25  
According to the present invention, there is provided a magnetic marker or tag which is characterised by a substrate carrying a plurality of discrete magnetically active regions disposed in one or  
30 more linear arrays, the magnetically active regions being formed of a thin film or spin-melt material having a preferential axis of magnetisation, and the preferential axes of magnetisation being aligned within the (or each) linear array.

35

The preferential axes of magnetisation in tags of

this invention may be generated by longitudinal annealing of a spin-melt material. The discrete magnetically active regions may be formed from a continuous area of magnetisable material discrete  
5 regions of which are magnetised and to generate space(s) between said magnetically active regions.

The magnetically active regions of the tag may comprise two linear arrays disposed orthogonally.  
10

Advantageously, the tag is in the form of a relatively long, thin strip having a preferential axis of magnetisation along its length.

15 In one embodiment of the tag of this invention, either the magnetically active regions, or the spaces between said magnetically active regions, or both, is or are non-uniform.

20 If desired, each of the magnetically active regions may be of substantially the same shape and size. Also, the spacing between each of the magnetically active regions may, if desired, be uniform; it may alternatively be non-uniform.

25 The magnetic interrogation systems described in the PCT application can function with magnetic tags which are characterised by carrying a plurality of discrete magnetically active regions in a linear array.

30 The discrete magnetically active regions may be supported on a substrate, e.g. paper or a plastics material, or they may be self-supporting. Alternatively, the magnetic elements may be incorporated directed into or onto articles during  
35 manufacture of the articles themselves. This is appropriate, for example, when the articles are goods,



e.g. retail goods, which carry the tags for inventory purposes; or when the articles are tickets or security passes.

5       A tag as described above can also be formed from a continuous strip of high permeability material, discrete regions of which have their magnetic properties permanently or temporarily modified. It will be appreciated that such a process can begin with  
10 a high permeability strip selected regions of which are then treated so as to modify their magnetic properties, generally by removing or reducing their magnetic permeability; or with a strip of high permeability magnetic material accompanied by a magnetisable strip  
15 positioned close to the high permeability magnetic material, e.g. overlying it or adjacent to it, selected regions of which are magnetised. In relatively simple embodiments, each magnetically active region has the same magnetic characteristics; in more complex  
20 embodiments, each magnetically active region can possess a different magnetic characteristic, thus making it possible to assemble a large number of tags each with unique magnetic properties and hence with a unique magnetic identity and signature (when processed  
25 by a suitable reader device).

Because the invention of the parent application . utilises relative movement between a tag and an applied magnetic field, it will be appreciated that there will  
30 be a correspondence between the time domain of output signals from a tag reading device and the linear dimensions of the magnetically active regions of a tag and of the gaps between the magnetically active regions. In this sense, the active regions and the  
35 gaps between them function analogously to the elements of an optical bar code (black bar or white gap between

adjacent bars). It follows from this that, just as variability of magnetic characteristics in the active regions can be used to generate part of a tag "identity", so can the linear spacing between adjacent  
5 magnetically active regions. It will readily be understood that a vast number of tags, each with its own unique identity, can thus be produced.

Although the tags have been described as  
10 possessing a linear array of magnetically active regions, the tags may in fact have two or more such linear arrays. These may be disposed mutually parallel, or mutually orthogonal, or in any desired geometrical arrangement. For simplicity of reading  
15 such tags, arrays which are parallel and/or orthogonal are preferred.

Appropriate techniques for manufacturing the tags just described are well-known in conventional label  
20 (i.e. magnetic marker) manufacture. Suitable magnetic materials are also well-known and widely available; they are high-permeability materials which preferably have an extrinsic relative permeability of at least  $10^3$ . The coercivity of the magnetic material will  
25 depend on the tag's intended use. The magnetic material is preferably in the form of a long thin strip or of a thin film; these formats avoid major internal demagnetisation effects. Suitable strip materials are readily available from commercial suppliers such as  
30 Vacuumschmeltze (Germany), Allied Signal Corp. (USA), and Unitika (Japan). Thin film material currently manufactured in high volume by IST (Belgium) for retail security tag applications is also suitable for use.

35 In the magnetic interrogation techniques described in the PCT application, the magnetic null is preferably

caused to sweep back and forth over a predetermined region within the interrogation zone. The scanning frequency (i.e. the sweep frequency of the magnetic null) is preferably relatively low, e.g. 1 - 500Hz.

- 5 Conveniently, the field pattern is arranged so that (a) said magnetic null lies in a plane; and (b) the saturating field occurs adjacent to said plane.

- 10 The relative movement between the magnetic element and the magnetic field may advantageously be produced by sweeping the applied magnetic field over the magnetic element. Alternatively, the relative movement can be achieved by the application of an alternating magnetic field to a generally static magnetic field  
15 pattern.

- In carrying out the methods described above, preferred embodiments of the magnetic element are either elongate, and the magnetic null is then arranged  
20 to extend along the major axis of said magnetic element; or they are in the form of a thin film, in which case the magnetic null is arranged to extend to be aligned with the axis of magnetic sensitivity of the thin film material.  
25

- The magnetic field or field pattern utilised in the methods described above may be established by the means of two magnetic fields of opposite polarity. This can conveniently be achieved by use of one or more  
30 coils carrying direct current; or by the use of one or more permanent magnets; or by a combination of coil(s) and magnet(s).

- Where a coil is used, it may be arranged to carry  
35 a substantially constant current so as to maintain the magnetic null at a fixed point. Alternatively, the

coil(s) carry/carries a current whose magnitude varies in a predetermined cycle so that the position of the magnetic null is caused to oscillate in a predetermined manner. We describe this as a "flying null". A  
5 similar arrangement can be used to give a flying null when both a coil or coils and a permanent magnet are used.

Relative movement between the magnetic field and  
10 the magnetic element may be achieved by applying a relatively low amplitude alternating magnetic field superimposed on the DC field. Typically, such a low amplitude alternating magnetic field has a frequency in the range from 10Hz to 100kHz, preferably from 50Hz to  
15 50kHz, and most advantageously from 500Hz to 5kHz.

In one embodiment, the coils carry a substantially constant current so as to maintain the magnetic null at a fixed point. In another embodiment, the coils carry  
20 a current whose amplitude varies in a predetermined cycle so that the position of the magnetic null is caused to oscillate in a predetermined manner.

In the methods described above, detection of the  
25 magnetic response of the magnetic element advantageously comprises observation of harmonics of the applied AC field which are generated by the magnetic element as its magnetisation state is altered by passing through the magnetic null.

30

As indicated above, the methods operates with a zero or very low frequency scanning field, and an HF (high frequency) in the range 50Hz - 50kHz. This allows for good signal penetration through most  
35 materials including thin metal foils. In addition, international regulations allow high fields for

transmission at these low frequencies.

These interrogation methods may thus provide a multi-bit data tag system which employs low-frequency  
5 inductive magnetic interrogation, and avoids the need for complex, expensive tags.

Before describing the present invention, it will be helpful to explain some fundamental aspects of the  
10 interrogation system described in the PCT application giving reference, where appropriate, to relatively simple embodiments.

A key aspect of the interrogation system is the  
15 form of the magnetic field created in the interrogation zone; as will become apparent later, this field allows very small spatial regions to be interrogated. The means for generating this magnetic field will be termed hereinafter an "interrogator". In one simple form, the  
20 interrogator consists of a pair of closely-spaced identical coils arranged with their axes coincident. The coils are connected together such that their winding directions are opposed in sense, and a DC current is passed through them. This causes opposing  
25 magnetic fields to be set up on the coils axis, such that a position of zero field - a magnetic null - is created along the coil axis, mid-way between the coils. The level of current in the coils is such as to heavily saturate a small sample of high permeability magnetic  
30 material placed at the centre of either of the two coils. A much lower amplitude AC current is also caused to flow in opposite directions through the two coils, so that the AC fields produced sum together mid-way between the coils. This can easily be arranged by  
35 connecting a suitable current source to the junction of the two coils, with a ground return. The frequency of

this AC current may typically be about 2 kHz, but its value is not critical, and suitable frequencies extend over a wide range. This AC current generates the interrogating field which interacts with a magnetic tag to generate a detectable response. Another effect of this AC current is to cause the position of zero field - the magnetic null - to oscillate about the mid-way position along the coils axis by a small amount (this is a wobble or oscillation rather than an excursion of any significant extent).

In addition, a further, low frequency AC current may be fed to the coils so as to generate a low frequency scanning field (which may be zero). The frequency of the scanning field (when present) should be sufficiently low to allow many cycles of the relatively high frequency interrogation field to occur in the time that the magnetic null region passes over the tag; typically, the frequency ratio of interrogating field ( $\omega_c$ ) to the scanning field ( $\omega_p$ ) is of the order of 100:1, although it will be appreciated that this ratio can vary over a considerable range without there being any deleterious effect on the performance of the technique.

When a tag containing a piece of high-permeability magnetic material is passed along the coils axis through the region over which oscillation of the magnetic zero plane occurs, it will initially be completely saturated by the DC magnetic field. It will next briefly be driven over its B-H loop as it passes through the zero field region. Finally it will become saturated again. The region over which the magnetic material is "active", i.e. is undergoing magnetic changes, will be physically small, and is determined by the amplitude of the DC field, the amplitude of the AC

field, and the characteristics of the magnetic material. This region can easily be less than 1 mm in extent. If the level of the alternating field is well below that required to saturate the magnetic material

5 in the tag, then harmonics of the AC signal will be generated by the tag as it enters the zero field region of interrogator field and responds to the changing field. As the tag straddles the narrow zero field region the tag will be driven on the linear part of its

10 B-H loop, and will interact by re-radiating only the fundamental interrogation frequency. Then, as the tag leaves the zero field region, it will again emit harmonics of the interrogation field frequency. A receiver coil arranged to be sensitive to fields

15 produced at the zero field region, but which does not couple directly to the interrogator coils, will receive only these signals. The variation of these signals with time as the tag passes along the coils axis gives a clear indication of the passage of the ends of the

20 magnetic material through the zero field region.

It will be appreciated that because the interrogation zone can be very narrow, each individual piece of magnetic material can be distinguished from

25 its neighbours, from which it is separated by a small distance. Naturally, the magnetic material will be selected to suit the particular application for which the tag is intended. Suitable magnetic materials are commercially available, as described hereinbefore.

30

If a tag containing a number of zones or pieces of magnetic material placed along the axis of the label is now considered, it will be appreciated that as each zone or piece of magnetic material passes through the

35 zero-field region, its presence and the positions of its ends can be detected. It then becomes a simple

matter to use the lengths and spacings of individual zones or pieces of magnetic material to represent particular code sequences. Many different coding schemes are possible: one efficient arrangement is to  
5 use an analogue of the coding scheme used for optical barcodes, where data is represented by the spacing and widths of the lines in the code.

The system so far described allows for the  
10 scanning of a single-axis tag (e.g. a wire or a thin strip of anisotropic material, having a magnetic axis along its length) as it physically moves through the coil assembly. It will be appreciated that relative movement between the tag and the interrogating field  
15 can be achieved either with the field stationary and the tag moving, or vice versa. If required, the arrangement can be made self-scanning, and thus able to interrogate a stationary tag, e.g. by modulating the d.c. drive currents to the two interrogator coils, so  
20 that the zero field region scans over an appropriate portion of the axis of the coils. The extent of this oscillation needs to be at least equal to the maximum dimension of a tag, and should preferably be considerably greater, to avoid the need for precise tag  
25 positioning within the interrogation zone.

By using extra coils arranged on the 2 axes orthogonal to the original, tags in random orientations  
30 can be read by sequentially field scanning. This involves much greater complexity in the correlation of signals from the three planes, but because of the very high spatial resolution available would be capable of reading many tags simultaneously present in a common  
35 interrogation volume. This is of enormous benefit for applications such as tagging everyday retail shopping



items, and, for example, would allow automated price totalisation of a bag of shopping at the point of sale. Thus the technique has applicability to the price labelling of articles and to point-of-sale systems  
5 which generate a sales total (with or without accompanying inventory-related data processing).

The size of a simple linear tag is dependent on the length of the individual elements, their spacing  
10 and the number of data bits required. Using strips of the highest permeability material commercially available, such as the "spin-melt" alloy foils available from suppliers such as Vacuumschmeltze (Germany) and Allied Signal (USA), the minimum length  
15 of individual elements which can be used is probably of the order of a few millimetres. This is because the extrinsic permeability will be dominated by shape factors rather than by the very high intrinsic permeability (typically  $10^5$ ), and shorter lengths may  
20 have insufficient permeability for satisfactory operation.

For this reason it is attractive to use very thin films of high permeability magnetic material. Provided  
25 it is very thin, (ideally less than  $1\mu\text{m}$ ), such material can be cut into small 2 dimensional pieces (squares, discs etc) with areas of just  $20\text{ mm}^2$  or less, yet still retain high permeability. This will enable shorter tags than possible with elements made from commercially  
30 available high-permeability foils. Suitable thin film materials are available commercially from IST (Belgium).

An extension to this type of programming can also  
35 be used to prevent the composite tag producing an alarm in a retail security system (such an alarm would be a

false indication of theft, and would thus be an embarrassment both to the retailer and to the purchaser). If different regions of the tag are biased with different static field levels, they will produce  
5 signals at different times when they pass through retail security systems. This will complicate the label signature in such systems and prevent an alarm being caused. In the present technique, the reading system will be able to handle the time-shifted signals  
10 caused by such magnetic biasing.

Thus far tag coding has been described on the basis of physically separated magnetic elements. It is not essential, however, to physically separate the  
15 elements; programming of data onto a tag may be accomplished by destroying the high-permeability properties of a continuous magnetic element in selected regions thereof. This can be done, for example, by local heating to above the recrystallisation  
20 temperature of the amorphous alloy, or by stamping or otherwise working the material. Of even more importance is the ability to magnetically isolate regions of a continuous element of high permeability material by means of a magnetic pattern stored on an  
25 adjacent bias element made from medium or high coercivity magnetic material. Such a composite tag could then be simply coded by writing a magnetic pattern onto the bias element using a suitable magnetic recording head. If required, the tag could then be  
30 erased (by de-gaussing with an AC field) and re-programmed with new data.

The scheme described can also be extended to operate with tags storing data in two dimensions. This  
35 allows for much more compact tags, since as well as being a more convenient form, a tag made up from an  $N \times$

N array of thin-film patches has much more coding potential than a linear array of the same number of patches. This is because there are many more unique patch inter-relationships that can be set up in a given  
5 area.

Advantageously, the small piece of high permeability magnetic material is in the form of a thin foil, a wire or a thin film.  
10

In addition to interrogating space to read data tags, the new technique of moving planes of zero field through space (or moving things through the planes) can be used to provide accurate location information for  
15 small items of high permeability magnetic material.

Thus it is possible to use this technique to determine the precise location of an object. This is of particular interest when the object whose location  
20 is to be determine is a surgical instrument, for example a surgical probe or needle. The technique allows precise determination of the location of, for example, a surgical probe during an operation.

25 This technique is ideal for accurate location of very small markers within relatively confined volumes; it can separately resolve multiple markers. It also displays low sensitivity to extraneous metal objects.

30 The magnetic tag or marker can typically be a 1 cm length (longer if desired) of amorphous wire (non-corrosive, diameter 90 micron or less) similar to that used in EAS tags or, with suitable process development, a short length (eg 1 cm) of a needle sputter-coated  
35 with a thin layer of soft magnetic material.

In use around the head of a patient, resolution to 0.1 mm with the described markers can be achieved. accuracy should also have the potential to approach this value if some precautions about calibration and use of other magnetic materials are observed, but for optimum performance a rigid but open structure close to the head would be desired. The magnetic field levels employed will be lower than those generated by every day magnets (eg kitchen door catches etc).

10

This technique has particular application to brain surgery, where there is the requirement to locate the position of probes in three dimensions and with high precision. It is therefore possible, in accordance with this invention, to use small magnetic markers on such probes or needles. In this case, a key advantage is that the signal from the marker need only be detected and resolved in time; the resolution is determined by the location of the zero field plane, not by the signal to noise ratio of the detected marker signal. This permits a very small marker to be used.

A single axis position sensor may be implemented with a set of coils similar to the tag reading system described above. This comprises: a pair of opposed coils carrying DC current to generate a DC field gradient; a means of applying a relatively uniform low level AC field to drive the marker in and out of saturation in the small region where the DC field is close to zero; and a means of applying a relatively uniform DC field of variable strength and polarity to move the location of the plane of zero DC field around the volume to be interrogated.

35        An anisotropic marker - i.e. one having a preferential axis of magnetisation - resolves the

magnetic field along its length. Such a marker can be obtained, for example, by using a long, thin element of a magnetic material or by suitable treatment of an area of magnetic material having a much lower aspect ratio, e.g. by longitudinally annealing a generally rectangular patch of a spin-melt magnetic material. In the context of the single axis position sensor under discussion there are five degrees of freedom (x,y,z and two angles (rotation of the marker about its axis has no effect)). Three orthogonal complete sets of coils can capture sufficient information by doing three scans of the uniform DC field on each of the sets of coils in turn. The first scan with no field from the other sets, the second with a uniform DC field from one of the other sets, and the third with DC field from the other set. This gives nine scans in all; these may be represented as in the following table, in which the magnetic field sources are identified as a, b and c and the scans are numbered from 1-9 (scanning order being of no significance):

Orthogonal field source	1	2	3	4	5	6	7	8	9
a	ON	ON	ON	OFF	OFF	ON	OFF	OFF	ON
b	OFF	ON	OFF	ON	ON	ON	OFF	ON	OFF
c	OFF	OFF	ON	OFF	ON	OFF	ON	ON	ON

The only information required from each scan is the position of the centre of the harmonic output from the marker within that scan. These nine DC field values can then be converted into the xyz-theta-phi co-ordinates of the marker. To start with, the system can simply be used by holding the marker in the desired position before the head is put into the coils; and then when the head is placed in the coils the marker

can be moved until the same signals are obtained.

An alternative to sequential interrogation which has the advantage of requiring less time to scan the region of interest is to rotate the magnetic field gradient continuously so as to scan all directions of interest. This can be accomplished by driving three sets of coils with appropriate continuous waveforms. For example, a suitable scanning field will be created if coils in the x, y and z planes are driven with currents  $I_x$ ,  $I_y$  and  $I_z$  given by the equations:

$$\begin{aligned} I_x &= \cos \omega_a t (A \cos \omega_b t - \sin \omega_b t \sin \omega_c t) \\ &\quad - \sin \omega_a t \cos \omega_c t \\ I_y &= \sin \omega_a t (A \cos \omega_b t - \sin \omega_b t \sin \omega_c t) \\ &\quad + \cos \omega_a t \cos \omega_c t \\ I_z &= A \sin \omega_b t + \cos \omega_b t \sin \omega_c t \end{aligned}$$

where:  $\omega_a$  = overall frequency of rotation of applied magnetic field  
 $\omega_b$  = null scanning frequency  
 $\omega_c$  = interrogation frequency  
 $A$  = amplitude ratio  $\omega_b : \omega_c$ .

Typical (but non-limiting) values of these parameters are:  $A \approx 10$ ;

frequency ratio  $\omega_a : \omega_b \approx 1 : 10$ ; and

frequency ratio  $\omega_b : \omega_c \approx 1 : 400$ .

The invention will now be illustrated with reference to the accompanying drawings, in which:

FIGURE 1 illustrates the fundamental elements of a tag reading system of the parent application;

FIGURE 2 is a circuit diagram illustrating one

mode of generating the desired magnetic field pattern with the arrangement of Fig. 1;

FIGURE 3 relates the magnetic response of a tag to its position within the reading system of Fig. 1;

5       FIGURE 4 illustrates where magnetic nulls occur with a permanent magnet;

FIGURE 5 illustrates an embodiment of the invention which utilises a coil and a permanent magnet to generate the desired field pattern;

10       FIGURE 6 illustrates the use of a pair of permanent magnets to generate the desired field pattern;

FIGURE 7 illustrates the use of a plurality of permanent magnets disposed in an annular array with a  
15       coil to generate the desired field pattern;

FIGURE 8 is a schematic circuit diagram for one embodiment of a tag interrogator;

FIGURE 9 illustrates a selection of tags in accordance with this invention; and

20       FIGURE 10 illustrates an application of the magnetic interrogation technique as applied to surgical operations.

Referring to Figure 1, a schematic arrangement is  
25       shown in which a tag 1 is positioned mid-way between two coils Tx1 and Tx2. The tag is of the type shown in Figure 9a, i.e. a simple linear tag carrying a plurality of magnetic elements each of which is a high-permeability magnetic alloy material, for example  
30       Vacuumschmeltze 6025 spin melt ribbon having an intrinsic permeability of about  $10^5$ . The reader will appreciate that the values given in this description for the various parameters associated with the elements shown in Figure 1 are given merely by way of example,  
35       and illustrate one working embodiment. The values of these parameters will inevitably vary according to the

overall size of the system and its intended function. The magnetic elements which constitute the discrete magnetically active regions of the tag have dimensions 10mm x 1mm x 25 microns; the spacing between adjacent  
5 elements is 1mm. The two coils are spaced apart by approximately 20cm and each comprise 450 turns of 0.56mm copper wire wound in a square configuration typically 45cm x 45cm. Each coil has a resistance of 6 $\Omega$  and an inductance of 100mH. Each of the coils Tx1  
10 and Tx2 carries a direct current  $I$  superimposed upon which is a smaller alternating current  $i$ ; typically, the direct current  $I$  is of the order of 3A while the superimposed alternating current  $i$  is of the order of 50mA. The alternating current  $i$  is of relatively high  
15 frequency, typically about 2kHz.

With a system such as that just described, the alternating and direct currents in the two coils generate a magnetic field pattern in which there is a  
20 magnetic null in the direction of arrow  $x$  at points lying in a plane parallel to the two coils and mid-way between them. In Figure 1, the x- and y-coordinates of this mid-way plane are represented by the lines 2 and 3, respectively.

25

If a magnetic tag of this invention is passed through the two coils shown in Figure 1, travelling in direction  $x$  and generally along the longitudinal axis defined between the centre points of the two coils, it  
30 will pass through a magnetic field polarity inversion at the mid-way plane defined by coordinates 2 and 3. The change in polarity of the magnetic field comes about because the DC current flows in one sense in the first of the coils and in the opposite sense in the  
35 other of the coils, as indicated by the bold arrows in Figure 1. At the mid-way plane, the magnetic field



component generated by the direct current flowing in the first coil exactly cancels the magnetic field component generated by the direct current flowing in the other coil.

5

As the tag travels through the centre of the first coil, it experiences a high magnetic field which is sufficient to saturate its magnetically active elements; as the field strength decreases on moving  
10 towards the mid-way plane, the magnetic material is influenced by the decreasing magnetic field in a way dictated by its hysteresis curve. In the vicinity of the magnetic null, the direction of magnetisation of the magnetic elements of the tag is reversed.

15

The relatively high frequency alternating current i shown in Figure 1 is identical in each of the coils Tx1 and Tx2.

20

The alternating current can have a frequency within a wide range, as indicated hereinbefore; a typical operating value with the arrangement of Figure 1 is about 2kHz. The effect of this relatively low amplitude alternating current is to cause the mid-way  
25 plane defined by coordinates 2, 3 to oscillate about the geometric midpoint along the longitudinal axis defined between the midpoints of the two coils. In other words, the plane containing the magnetic null oscillates or wobbles back and forth over a small  
30 spatial region at the frequency of the alternating current.

Figure 2 shows a simple circuit for providing opposed DC fields combined with AC fields. Capacitor  
35 C1 is selected to resonate with the inductance of coils Tx1 and Tx2 at the AC drive frequency; each of these

coils has a resistance of 6 ohms and an inductance of 100 millihenries. A typical value for C1 is 0.1 $\mu$ F. C2 is a capacitor selected to behave as an effective short-circuit at the AC drive frequency; a typical  
5 value for this component is 22 $\mu$ F. The DC power supply will typically provide 30 volts at 3 amps; and the AC source will typically deliver an alternating current at a frequency of 2kHz at 2v rms.

10 Figure 3 illustrates how the magnetisation of a single magnetic element varies with time at different positions within the magnetic field pattern defined between the coils Tx1 and Tx2 of Figure 1. For ease of illustration, the oscillation of the plane containing  
15 the magnetic null is represented by the bold double-headed arrow ( $\leftrightarrow$ ) 4, the extreme positions of the plane being represented by dashed lines 5 and 6, respectively, and the mid-point between limiting planes 5 and 6 being represented by dashed line 7. In the  
20 right hand portion of Figure 3, the applied AC field is shown varying with time between positive (H+) and negative (H-) field values. Beneath the graph of the applied AC field, there are five graphs depicting how the net magnetisation of the magnetic element varies  
25 with time in each of five geometric positions indicated to the left as Position 1, Position 2, etc. Planes 5 and 6 define the limits of regions within which magnetic field polarity reversals occur. In practice, the separation between planes 5 and 6 is typically of  
30 the order of 1 mm; for a given magnetic material, this distance can be increased or decreased at will within certain limits by varying the amplitude of the AC current and/or the DC current in the coils.

35 At all times, the magnetic element has a linear

magnetic axis which is orthogonal to the planes 5, 6 and 7.

In Position 1, the end of the magnetic element is  
5 adjacent to plane 6; in this condition, it experiences  
a positive magnetic field at all times and its net  
magnetisation is time-invariant. In Position 2, the  
leading end of the element has reached the mid-way  
plane 7. Most of the magnetic material, however, still  
10 remains outside limiting plane 6. In consequence, the  
null plane is able to interact with only a portion of  
the magnetic material, resulting in a time-variable net  
magnetisation having the repeat pattern shown, i.e. a  
straight line positive-value portion followed by a  
15 generally sinusoidal arc which dips towards zero and  
then rises to its original positive value.

In Position 3, the magnetic material is positioned  
symmetrically with respect to the mid-way plane 7.  
20 Here, the net magnetisation versus time plot consists  
of a sine wave whose frequency corresponds to that of  
the applied AC field. In Position 4, the majority of  
the magnetic element experiences a negative field at  
all times, while a smaller part of the element  
25 experiences polarity reversals; this leads to the net  
magnetisation versus time plot as shown. The fact that  
Position 4 is in effect the inverse of Position 2 is  
reflected in the relationship between the magnetisation  
plots for these two positions; as can be seen, the plot  
30 for Position 4 is effectively a mirror image of that  
for Position 2 but with the curved portions time-  
shifted.

Finally, that Position 5, all of the tag  
35 experiences the negative field, and no part of the tag  
experiences field polarity reversal. In consequence,

the net magnetisation is time-invariant, being a constant negative value as shown.

When a tag containing such a magnetic element is  
5 passed along the coils' axis through the region of zero  
field, it will initially be completely saturated by the  
DC magnetic field. It will next briefly be driven over  
its B-H loop as it passes through the zero field  
region. Finally it will become saturated again. The  
10 portion of the traverse over which the magnetic  
material is "active", i.e. is undergoing magnetic  
changes, is physically small, and is determined by the  
amplitude of the DC field, the amplitude of the AC  
field, and the characteristics of the magnetic  
15 material. This region can easily be less than 1mm in  
extent. If the level of the alternating field is well  
below that required to saturate the magnetic material  
in the tag, then harmonics of the AC signal will be  
generated by the tag as it enters the zero field region  
20 (Positions 1 to 2) and responds to the changing field.  
As the tag straddles the narrow zero field region  
(Position 3) the tag will be driven on the linear part  
of its B-H loop, and will interact by re-radiating only  
the fundamental interrogation frequency. Then, as the  
25 tag leaves the zero field region, (Positions 4 to 5) it  
will again emit harmonics of the interrogation field  
frequency.

A receiver (Rx) coil arranged to be sensitive to  
30 fields produced at the zero field region, but which  
does not couple directly to the interrogator (Tx)  
coils, will receive only these signals. Such an  
arrangement can be achieved by using separate Tx and Rx  
coils physically arranged to have low mutual coupling;  
35 or by using a single coil (having both Tx and Rx  
functions) together with suitable filtering in the Tx

and Rx paths. The variation of these signals with time as the tag passes along the coils' axis gives a clear indication of the passage of the ends of the magnetic material through the zero field region.

5

The result of this interaction between the tag and the magnetic field it experiences is shown in Figure 3b. Here, the region 4 over which the magnetic null oscillates is shown on a smaller scale, and the  
10 numbered dots represent the location of the mid-point of the tag in each of Positions 1-5. The generation of a harmonic signal by the tag (illustrated by the second harmonic of the applied frequency) is apparent at  
15 positions where the tag enters the region defined by limiting planes 5 and 6, i.e. the zone where magnetic field polarity reversals occur. Because of the symmetry of the system, a single magnetic element will generate a doublet peak 8a and 8b since Positions 2 and 4 are redundant.

20

Referring now to Figure 4, this illustrates the lines of force (i.e. the magnetic contours) existing with a simple bar magnet. The plane X-Y which  
25 intersects the longitudinal axis of the bar magnet and which is orthogonal to the plane of the paper constitutes a magnetic null plane. Thus a magnetic element possessing a sensitive magnetic axis aligned  
orthogonally with respect to the null plane will experience a magnetic null as it traverses either path  
30 A-B or path C-D. Consequently a simple bar magnet can be used as part of an interrogation system to detect the presence of such a magnetic tag, or to read information carried by such a tag.

35

The generation of second harmonic signal can form the basis of a tag detection system. If, instead of

just a single magnetic element, the tag includes a linear array of  $n$  magnetic elements, the second harmonic output from the tag will comprise  $n$  duplet peaks, each of the type shown in Figure 3b. If the

5 size and magnetic characteristics of the magnetic elements are all the same, the peaks will have the same profile and each peak will define an envelope of constant area. The spacing between individual magnetic elements will influence the relative positions of the

10 duplet peaks on an amplitude versus time plot. It will be appreciated that the present invention is not restricted to the use of such simple tags as just described. The use of magnetic elements of different

15 sizes and magnetic characteristics, and with non-uniform spacing along the length of the magnetic tag, will generate more complex signal patterns which nevertheless are characteristic of the given tag construction. By varying the number, the magnetic

20 characteristics, and the positioning of a series of magnetic elements, it is possible to manufacture a very large number of magnetic tags each with its own unique characteristics which will accordingly generate a unique signal when used in conjunction with the system of Figures 1-3.

25

It will also be appreciated that the magnetic interrogation technique is not limited to observing the second harmonic of the applied alternating frequency; this particular harmonic has been selected for the

30 purposes of illustration since it is relatively easy to generate a transmit signal (Tx output) which has no (or very little) second harmonic content, thus permitting good discrimination between the Tx signal and the response of the tag; and since it also contains a

35 relatively high proportion of the total harmonic energy output from the tag.

Referring next to Figure 5, there is shown a schematic arrangement for a simple tag reader, the reader utilising a permanent magnet 10 and a coil 11 located adjacent to one face of the magnet. In this embodiment, a tag which is to be read can be passed along path C-D through coil 11 or along path A-B above the coil. The tags must be oriented with their magnetic axis aligned with the direction of tag movement. In Figure 5, the magnetic null plane is positioned at 12 as shown.

Referring next to Figure 6, the use of two permanent magnets positioned with their magnetic axes aligned and with like poles opposing one another is illustrated. Such an arrangement generates a null plane 13; the direction of tag motion required is indicated by arrows 14. Again, the magnetic axis of the tag must be aligned with the direction of movement.

Figure 7 shows a simple realisation of a tag reader head using a plurality of permanent magnets to generate a magnetic null plane. As illustrated, ten polymer-bonded ferrite magnets are disposed in an annular array with like poles facing inwards. A common transmit/receive coil L1 sits within the annulus of magnets in the manner indicated. The tag is read as it passes through the null plane in the centre of the loop of magnets.

Referring next to Figure 8, there is shown one embodiment of an interrogation system which may be used in conjunction with tags of this invention. This is based on the use of a single coil L1 to act as both transmitter (Tx) coil, which generates the desired magnetic field pattern, and as the receiver (Rx) coil. The system uses the second harmonic output of the tag

as the basis for tag detection/identification. Circuit components C1 and L2 form a resonant trap at frequency  $2f$  to reduce signals at this frequency in the Tx output to a very low level; C2 resonates with L1 at frequency  $f$ ; and components C3, C4, L1 and L3 form a filter to pass wanted signals from the tag at frequency  $2f$  while rejecting signals at the transmitted frequency  $f$ .

The output obtained from this circuit passes through a low pass filter to an analogue to digital converter (ADC) and thence to a digital signal processor. These components, and in particular the signal processor, will be configured to suit the intended application of the interrogation unit. The nature of the signal processing, and the means by which it is achieved, are all conventional and therefore will not be described further here.

Figure 9 illustrates the basic structure of magnetic tags in accordance with the invention. Fig. 9a shows a tag 100 which comprises a support medium 101 (e.g. paper or a plastics material) and a linear array of magnetically active regions 102, 103, 104, 105 and 106. Each magnetically active region is formed from a patch of high-permeability magnetic material (e.g. Vacuumschmelze 6025) having its magnetic axis aligned along the length of the tag. Each patch is about  $10\text{mm}^2$  in area and is adhesively secured to the substrate 101.

Patches 101-105 are identical in dimensions and magnetic properties, and are uniformly spaced apart, gaps 110, 111 and 112 all being the same. The gap between patches 105 and 106, however, is larger - as though there were one patch missing at the position indicated by dotted lines at 113.



Tag 100 behaves as a six-bit tag, coded 111101 (the zero being area 113).

5 A functionally equivalent tag 120 is formed of a substrate 121 carrying magnetic elements 122-126 and having a "gap" 127; in this embodiment, the magnetic elements are in the form of a strip or wire of high-permeability magnetic material (e.g. Vacuumschmelze 6025), typically being about 5mm long, 1mm wide and  
10 about 15 microns in thickness.

Figure 9b illustrates an alternative construction for a six-bit, laminated tag 130. This tag is coded 111101, as in Fig. 9a. Here, a continuous layer or  
15 length of high permeability magnetic material 131 (in the form of wire, strip, thin film or foil) and a substrate 133 have sandwiched between them a magnetic bias layer 132. The bias layer is magnetised in predetermined areas which influence the overlying high  
20 permeability material to generate magnetically active regions indicated as 134, 135, 136, 137 and 138. Region 139 is not active, and thus constitutes a magnetic zero. When read by an interrogation system such as that of Fig. 8, the output generated by tags  
25 100, 120 and 130 will be as shown in Figure 9d.

A more complex tag is shown in Fig. 9c. Here there are a series of parallel linear arrays of magnetically active material, generating a 4 x 4 array  
30 of sites where the magnetically active material may be present (coding as '1') or absent (coding as '0').

Figure 10 illustrates the general arrangement of three sets of coils as used for surgical applications.  
35 The three sets of coils are all mutually orthogonal and define a cavity into which the head 200 of a patient

may be positioned. The first coil set consists of coils 201a and 201b; the second set consists of coils 202a and 202b; and the third set consists of coils 203a and 203b. In the drawing, two surgical probes 204 and 5 205 are shown schematically in position within the patient's cranium. The probes each have, at their distal ends, a magnetic tag 206, 207 such as one of those described with reference to Fig. 9 above. Because the magnetic element of the tag is only 10 required to provide information of its presence (rather than hold extensive data), relatively simple tags are preferred. A single magnetic element of high permeability magnetic material located at the tip of the probe is sufficient. The coils are operated in the 15 manner described in detail hereinabove. By utilising tags in accordance with the present invention, it is possible to determine the positions of the ends of the probes with high precision - and thus to carry out delicate surgical procedures with accuracy and with 20 minimum damage to healthy tissue.

CLAIMS:

1. A magnetic marker or tag which is characterised by a substrate carrying a plurality of discrete  
5 magnetically active regions disposed in one or more linear arrays, the magnetically active regions being formed of a thin film or spin-melt material having a preferential axis of magnetisation, and the preferential axes of magnetisation being aligned within  
10 the (or each) linear array.
2. A tag as claimed in claim 1, characterised in that either the magnetically active regions, or the spaces between said magnetically active regions, or both, is  
15 or are non-uniform.
3. A tag as claimed in claim 1 or 2, characterised in that the preferential axes of magnetisation are generated by longitudinal annealing of a spin-melt  
20 material.
4. A tag as claimed in claim 1, 2 or 3, characterised in that said discrete magnetically active regions are formed from a continuous area of magnetisable material  
25 discrete regions of which are magnetised and to generate space(s) between said magnetically active regions.
5. A tag as claimed in claim 1, 2, 3 or 4,  
30 characterised in that the tag has two linear arrays disposed orthogonally.
6. A tag as claimed in any one of claims 1 to 5, characterised in that it is in the form of a relatively  
35 long, thin strip having a preferential axis of magnetisation along its length.

7. A tag as claimed in claim 1, 3, 4, 5 or 6, characterised in that each of the magnetically active regions is of substantially the same shape and size.
- 5 8. A tag as claimed in claim 1, 3, 4, 5 or 6, characterised in that the spacing between each of the magnetically active regions is uniform.
9. A tag as claimed in claim 2, characterised in that
- 10 the spacing between each of the magnetically active regions is non-uniform.
10. A magnetic marker or tag as claimed in claim 1 and substantially as hereinbefore described.



INVESTOR IN PEOPLE

Application No: GB 0023923.6  
Claims searched: 1 to 15

Examiner: Jared Stokes  
Date of search: 28 June 2001

## Patents Act 1977 Search Report under Section 17

### Databases searched:

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:

UK Cl (Ed.S): H4L (LADMX)

Int Cl (Ed.7): G06K (19/06)

Other: On-Line - EPODOC, JAPIO, WPI

### Documents considered to be relevant:

Category	Identity of document and relevant passage	Relevant to claims
X	GB 2 322 049 A (Flying) See page 28 lines 18-24	1,2,4-5
X	EP 0 831 410 A2 (Flying) See abstract, column 4 lines 7-18	1
X	WO 00/08489 A1 (Flying) See page 10 lines 8-14	1,2
X	WO 99/28852 A1 (Technical) See page 14 line 7-page 16 line 10, figs 4b & 11	1,2,4-6, 9-12,14
X	WO98/26312 A1 (Flying) See page 3 lines 12-34	1,2,4,11, 12,13
X	US 5 834 748 (Litman) See column 9 line 66-column 10 line 55	1-7,9,10, 14
X	US 4 940 966 (Pettigrew et al.) See column 3 line 51-line 68, figs 3 & 4, claim 2	1,2,4-6, 14
X	DE 19 535 019 (Cardtec) See column 4 lines 29-62, WPI abstract accession No. 1997-193629	1,2,4,5

X	Document indicating lack of novelty or inventive step	A	Document indicating technological background and/or state of the art.
Y	Document indicating lack of inventive step if combined with one or more other documents of same category.	P	Document published on or after the declared priority date but before the filing date of this invention.
&	Member of the same patent family	E	Patent document published on or after, but with priority date earlier than, the filing date of this application.



Application No: GB 9801603.3  
Claims searched: all

Examiner: Nigel Hall  
Date of search: 25 June 1998

**Patents Act 1977**  
**Search Report under Section 17**

**Databases searched:**

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:

UK CI (Ed.P): H4L (LADMA, LADMX)

Int CI (Ed.6): G01V 15/00; G08B 13/24

Other: Online: WPI

**Documents considered to be relevant:**

Category	Identity of document and relevant passage	Relevant to claims
A	EP 0353040 A2 (THORN)	

X	Document indicating lack of novelty or inventive step	A	Document indicating technological background and/or state of the art.
Y	Document indicating lack of inventive step if combined with one or more other documents of same category.	P	Document published on or after the declared priority date but before the filing date of this invention.
&	Member of the same patent family	E	Patent document published on or after, but with priority date earlier than, the filing date of this application.